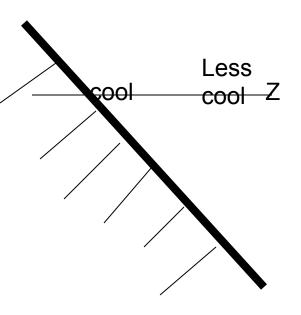
Slope and Valley winds

Another type of thermally-forced (or externally forced) mesoscale circulation → the slope wind, which is driven primarily by buoyancy (though it can be interpreted also in terms of PGF)



- Begin with an illustrative example: nocturnal slope flow, or katabatic flow (katabatic is a general term for downslope wind; the upslope counterpart is anabatic)
- Consider some height Z relative to sea level. Around sunset the land surface cools rapidly. At the same height Z but away from the terrain, the air cools relatively little. Thus, a parcel of air adjacent to the slope is negatively buoyant and will tend to accelerate downhill

Simplified solution for thermallydriven slope winds

- The following solution is similar to that developed by Prandtl (1942)
- Assume:
 - -- we have a 2D slope
 - -- time (space) scales are small enough to neglect the Coriolis force
 - -- steady state

- We will use a rotated coordinate system (s,n) with s pointed along the slope (positive downslope) and n directed normal to the slope. The slope angle above the horizontal plane is β , and the base state potential temperature stratification is $\delta = \partial \theta_0 / \partial z$ (note NOT $\partial \theta_0 / \partial z$)
- A simplified governing set of equations is:

U-momentum: $\partial u/\partial t = 0 = g\theta'/\theta_{00} \sin\beta + K_m \partial^2 u/\partial n^2$ Component of buoyancy along slope

friction

Thermodynamic equation:

$$\partial \theta' / \partial t = 0 = -u \sin \beta \delta + K_h \partial^2 \theta' / \partial n^2$$

Vertical advection of base-state θ by perturbation wind

Diffusion of θ

Notice the advection term is linear because it involves the advection of the base state θ by the perturbation wind. Since usin β =w where w is the cartesian vertical velocity, and δ = $\partial\theta_0$ / ∂ z, this term works out to -w $\partial\theta_0$ / ∂ z which is more familiar as vertical advection.

- Assume that the base state and terrain geometry are known and that we can specify K_m , K_h . Then we have 2 linear equations in two unknowns, u and θ , so we can look for a solution.
- Take $\partial^2/\partial n^2$ of the θ ' eq: $0 = -\partial^2 u/\partial n^2 \sin\beta\delta + K_h$ $\partial^4\theta$ ' $/\partial n^4$ (3)
- Solve the u eq. for $\partial^2 u/\partial n^2 = -g/K_m\theta'/\theta_{00}\sin\beta$ (4)
- And substitute into (3): $0 = (-g/K_m \theta'/\theta_{00} \sin\beta) \sin\theta\delta + K_h \partial^4 \theta'/\partial n^4$ (5)
- In (5), $g/\theta_{00}\delta = g/\theta_{00}\partial\theta_0/\partial z = N_0^2$ where N is the basic state Brunt-Vaisala frequency

• Then we can rewrite (5) as:

$$0 = N_0^2 / K_m \sin^2 \beta \theta' + K_h \partial^4 \theta' / \partial n^4$$
 (6)

Or
$$\partial^4 \theta' / \partial n^4 + N^2 \sin^2 \beta / K_m K_h \theta' = 0$$
 (7)

This is a 4th order differential equation for which the characteristic eqn is λ^4 + a = 0

The characteristic eqn can be factored into

$$(\lambda+b)(\lambda-b)(\lambda+ib)(\lambda-ib)$$

$$= (\lambda^2-b^2)(\lambda^2+b^2)$$

$$= \lambda^4 - b^4$$

Which corresponds to our characteristic eqn if we let $a = -b^4$ or $b = (-a)^{1/4} = -ia^{1/4}$

 Of the 4 roots, the only physical, bounded solution is

$$\theta'(n) = \theta_0' \cos(n/l) \exp(-n/l)$$

Where θ_0 ' is the potential temperature perturbation at the ground-air interface

$$I = (4K_mK_h/N^2\sin^2\beta)^{1/4}$$

Substituting θ' (n) into our original equation (and omitting extensive intermediate steps), we get...

$$u(n) = -g/N (K_m/K_h)-1/2 \theta_0'/\theta_{00} \sin(n/l)\exp(-n/l)$$

= $U(\theta_0')\sin(n/l)\exp(-n/l)$

Before computing numerical examples, let's look at the solution to get a general idea of the behavior:

Height variations:

- *superimposed exponential decay and periodic oscillation
- *the velocity has a jet-like profile: u=0 at n=0 (since sin(0)=0); increases to a maximum at some height above the surface, then decreases

- *find height of velocity maximum by setting ∂u/∂n = 0
- $U(\theta_0') \partial/\partial n[\sin(n/l)\exp(-n/l)] = 0$
- = $U(\theta_0')\partial/\partial n[\cos(n/l)\exp(-n/l)-\sin(n/l)\exp(-n/l)]$
- = $U(\theta_0')$ 1/I exp(-n/I) [cos(n/I) sin(n/I)]
- Thus we see that $\partial u/\partial n=0$ when $\cos(n/I)=\sin(n/I)$, which occurs at $n/I=\pi/4$, $5\pi/4$, $9\pi/4$, ...
- Given the exponential decay term, the highest value of u will be at the first value, $n=\pi/4$. Local max or min then occur at $5\pi/4$, $9\pi/4$, ...

- Above $n=\pi/l$, the solution reverses sign, and we have upslope flow; the sign of the flow reverses again above $n=2\pi l$, and so on.
- The value of the maximum velocity is then obtained by solving for n=πl/4:
- Umax = $U(\theta_0') \sin(\pi/4) \exp(-\pi/4)$ $\approx 0.32 \ U(\theta_0')$

• The intensity of the slope flow, $U(\theta_0')$, is linearly proportional to the intensity of surface cooling, θ_0 , and inversely proportional to the Brunt-Vaisala frequency, N, (i.e. the square root of the potential temperature gradient). The slope flow also is inversely proportional to the square root of the turbulent Prandtl number $(P_{rT} = K_m/K_h)$ but usually P_{rT} is close to 1 and varies only slightly (with stability).

Numerical example

- $\theta_0' = -5K$, $\theta = 288K$, $\partial \theta / \partial z = 9.8K$ km-1 (isothermal) so N≈0.018s-1, N²≈3x10-4s⁻²
- $\beta=5^{\circ} \rightarrow \sin\beta = 0.09$
- K_m=K_h=1 m2s⁻¹ (turbulent velocity scale ≈10 cm s⁻¹ and turbulent length scale of 10 m)
- Then $U(\theta_0') = (-9.8 \text{ms}^{-2}/0.018 \text{s}^{-1})(1)(5 \text{K}/288 \text{K}) = 9.4 \text{ ms}^{-1}$
- $I = (4*1m^2s^{-1}*1m^2s^{-1}/3x10-4s^{-2}*(0.09)^2)1/4 = 36m$
- The max slope flow velocity is when $n=\pi I/4$ or 28 m and equals 0.32 $U(\theta_0') = 3 \text{ ms}^{-1}$.